# Review of Deammonification projects and key results

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# **Real world wastewater technologies**

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Main-stream Deammonification Emerging technology

Side-stream Deammonification Emerged technology Established State of the Art

**Conventional N-removal** technologies

# **Side-stream applications**

- **DEMON-features** –
- pH-based process control
- cyclone for anammox enrichment
- DEMON-implementation More than 20 full-scale plants in Europe (A, Ger, SUI, Hu, NL, Serbia, SF,..) both municipal and industrial









#### **Incentive - resource savings**





#### Heidelberg / performance test, energy savings

![](_page_5_Figure_1.jpeg)

8,5 % less total energy consumption (per pe)

# applications

![](_page_6_Figure_1.jpeg)

# Industrial (2'400 kg N/d; yeast)

![](_page_7_Picture_1.jpeg)

### Landfill leachate

![](_page_8_Picture_1.jpeg)

![](_page_9_Picture_0.jpeg)

![](_page_9_Picture_1.jpeg)

#### Aquaculture

![](_page_10_Figure_1.jpeg)

effluent

#### trickling-filter

#### submerged-filter

screen

sludge-ca

# applications

![](_page_11_Figure_1.jpeg)

#### **WERF-Mainstream Deammonification Project**

#### **Objective of full-scale pilots**

• **Demonstration** projects at Strass WWTP and Glarnerland WWTP is to demonstrate the feasibility of the deammonification concept, which is already highly successful and proven in sidestream configurations at these plants, for the mainstream process.

• Using the fundamental process kinetics and the successful control mechanisms identified for NOB repression and anammox enrichment (Blue Plains bench scale pilots), process modeling was used to help identify the full scale demonstration strategy.

• Validation and advance the Blue Plains bench scale work. Data received from the trials will be systematically analyzed by calibration of a numerical model which facilitates understanding of the project results in a generic tool.

• Ultimately this model will help the design and implementation of this innovative technology.

# WERF-Project-Meeting 15th May 2012

#### **Mainstream Deammonification –**

#### **Basic process mechanisms**

- Competition for oxygen between AOB and NOB (controlled by DO-level and aeration time and -regimen)
- Competition for nitrite between NOB and Anammox (different nitrite half saturation and temperature sensitivity)

#### **Main process components**

- AOB Bioaugmentation and NOB Repression (Activity Measurements and Ko Determination)
- Anammox Bioaugmentation and Retention Efficiency (Activity Measurements and Particle Tracking)

#### **Operational data Strass**

![](_page_14_Figure_1.jpeg)

#### **Operational modes and -phases at the Strass pilot**

| cyclone set-up                                | date        | operation mode and DO set-points in tanks T1 and T2  |  |  |  |
|---|-------------|--|--|--|--|
| no cyclone                                    | before June | serial tanks: MLF.mode: T1 swing and T2=2.0  |  |  |  |
| batteries of small high-<br>pressure cyclones | 01.06.2011  | $3 \times 10^{\circ}$ ( $0 \times 3_{1}$ meetin/ $0 \times 1^{\circ}$ 11 $3 \times 10^{\circ}$ 12 $\times 2^{\circ}$ |  |  |  |
|   | 06.06.2011  | parallel tanks; T1=0.7 and T2=0.7  |  |  |  |
|   | 18.08.2011  | carial tanks: T1=0.5 and T2=0.7  |  |  |  |
| 2 large low-pressure<br>cyclones              | 06.09.2011  | Serial (anks, 11–0.5 and 12–0.)  |  |  |  |
|   | 29.09.2011  | serial tanks; T1=0.9 and T2=0.4  |  |  |  |
|   | 28.11.2011  | carial tanks: MLE mode: T1 aviag and T2-2.0  |  |  |  |
|   | 31.01.2012  | SCHALLAHINS, MLEHHOUC, TI SWILLY AND 12-2.0  |  |  |  |

![](_page_15_Figure_2.jpeg)

#### Hydro-cyclones Purpose – to seperate flocs (mainly AOB) and granules (mainly AMX) in order to select for different SRTs

![](_page_16_Picture_1.jpeg)

![](_page_17_Picture_0.jpeg)

#### Cyclone sizing and configuration

![](_page_18_Picture_1.jpeg)

Medium size Q=10m3/h per cyclor

![](_page_19_Picture_0.jpeg)

![](_page_20_Picture_0.jpeg)

![](_page_20_Figure_1.jpeg)

cyclone under-flow (recycled)

and overflow (wasted)

#### Spread-sheet models for systematic analyses of declining DO-tests

![](_page_21_Figure_1.jpeg)

Calibration of maximum growth-rates (linear range of depletion profile) and DO half saturation coefficients (curvature of profiles)

#### Image analyses based on particle size calculation color filtration

![](_page_22_Picture_1.jpeg)

Allows particle number counts, prticle size distribution and estimation of total volume or mass of anammox granules, respectively

![](_page_23_Figure_0.jpeg)

#### two most successful operation modes for NOB-repression (SND-type low DO and MLE-type high DO)

![](_page_24_Figure_0.jpeg)

Comparison of this year's and last year's operational data of the fullscale pilot Strass indicating advanced NOB-repression (typically high nitrate level at Christmas peak-load; similar temperature conditions of ca. 10°C, load conditions and ammonia effluent concentrations of ca. 2-5 mgN/L for both years)

![](_page_24_Figure_2.jpeg)

![](_page_25_Figure_0.jpeg)

![](_page_25_Figure_1.jpeg)

SVI-profiles (ml/g) and temperature (°C)

![](_page_26_Figure_0.jpeg)

#### Specific energy demand for nitrogen removal

The last samples show ammonia removal during anaerobic activity test (anammox activity)

![](_page_27_Figure_1.jpeg)

Only 25% of produced NOx from ammonia oxidation is converted to nitrate during aerobic activity test of the last sample

![](_page_27_Figure_3.jpeg)

![](_page_28_Figure_0.jpeg)

Comparison of maximum growth rates (left) and DO half saturation ko (right) of total nitrifiers (AOB+NOB) and NOB only calculated from measured DO depletion profiles of mainstream mixed liquor samples at 20°C and 30°C

![](_page_29_Figure_0.jpeg)

Evolution of the anammox biomass in the mainstream (B) from sampling one to twelve - distribution of granule size fraction.

![](_page_30_Figure_0.jpeg)

Abundance of granules mL<sup>-1</sup> and estimated granule volume mL<sup>-1</sup>

![](_page_31_Figure_0.jpeg)

Evolution of the anammox biomass of the mainstream cyclone underflow fraction (B-UF) from sampling one to twelve; distribution of granule size fraction (left); abundance of granules mL-1 (middle) and estimated granule volume mL-1 (right)

![](_page_32_Figure_0.jpeg)

Comparison of sidestream (PW) TSS and total granule volume in PWsamples over the sampling period

![](_page_33_Figure_0.jpeg)

Impact of intensive bioaugmentation out of the DEMON-reactor on its treatment performance

**Denaturing gradient gel of amplified Anammox 16S DNA gene** ragments of all B-samples (12 samplings at WWTP Strass) combined with PW-samples of three samplings (sampling 1, 6 and 12); M...Marker, P...PW-samples, numbers indicate the sampling time.

566 6M7 77 8 8 8PPP9 9 9 1010101

121212P PP

GHG-emissions (NO and N<sub>2</sub>O as intermediate products in N-removal)

one week campaign for measuring GHG emissions (N2O, NO, NO2, CH4, CO2) in order to compare carbon footprint before and after modifications in operation and to understand process implications on the gas phase

![](_page_35_Picture_2.jpeg)

# Model configuration of the original MLE-scheme (pre-denitrification tank represents 50% of volume; object of internal recirculation stream)

![](_page_36_Figure_1.jpeg)

# Model configuration of the new SND-scheme (aerated and anoxic zones are represented by 2 CSTR each; low DO operation)

![](_page_36_Figure_3.jpeg)

- Successful process operation and NOB repression depends on 2 parameters:
  - Competition between AOB and NOB for oxygen expressed by ko (here the same ko of 0.25 mgDO/L assumed)
  - Competition between Anammox and NOB for nitrite expressed by ks (default for Anammox ks=1.0 NO2-N/L; for NOB ks=0.1)

|   |    | biomass (mgCOD/L) |         |       | nitrogen (mgN/L) |       |  |
|---|----|-------------------|---------|-------|------------------|-------|--|
| process conditions & parameters                             |    | NOB               | Anammox | NH4-N | NO3-N            | NO2-N |  |
| <b>DOmax=0.35</b> ; ko=0.25; ks(NOB)=0.1; μmax(Anammox=0.1) | 40 | 21                | 35      | 2.6   | 3.9              | 0.61  |  |
| <b>DOmax=0.40</b> ; ko=0.25; ks(NOB)=0.1; μmax(Anammox=0.1) | 42 | 26                | 34      | 1.9   | 7.4              | 0.39  |  |
| DOmax=0.35; ko=0.25; ks(NOB)=0.1; <b>µmax(Anammox=0.0)</b>  | 42 | 27                | 30      | 2.9   | 6.9              | 0.72  |  |
| DOmax=0.35; ko=0.25; <b>ks(NOB)=0.5;</b> μmax(Anammox=0.1)  | 39 | 17                | 36      | 2.5   | 2.1              | 0.58  |  |

![](_page_38_Figure_0.jpeg)

#### **Overlap in Findings Bench-scale vs. Full-scale**

#### **Operation mode and aeration regime**

- Bench-scale reactor A (intermittent aeration) was more successful in NOB-repression and anammox enrichment compared to the continuously aerated control.
- During the full-scale testing, the intermittent aeration pattern (either along the flow-path or the time axis) creating transient anoxic conditions was found more effective for repressing NOBs.
- ko of NOB can adapt to low DO-conditions, therefore low-DO operation is not successful.

## **Process engineering fairy-tales**

Once upon a time there were nitrification and denitrification....